

Accelerometer Design Example

Analog Devices XL-05/50

Bernhard E. Boser

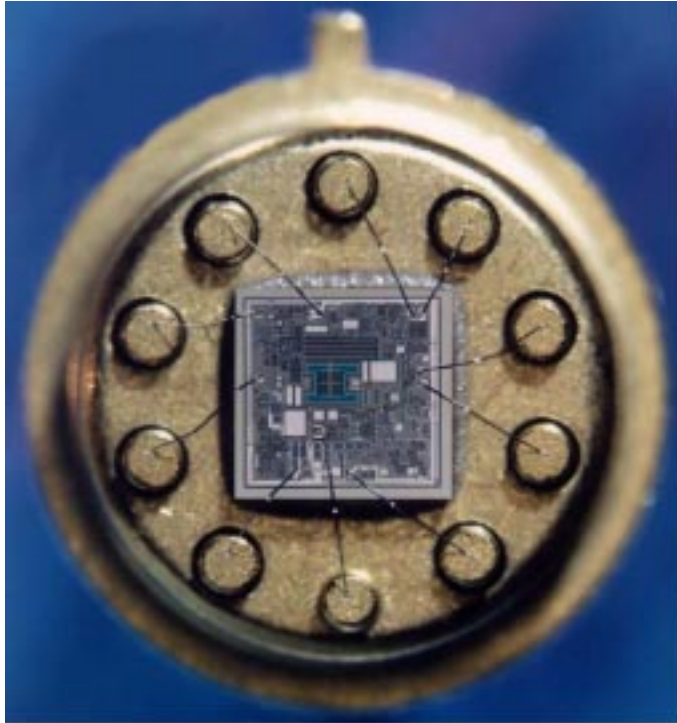
Berkeley Sensor & Actuator Center

Dept. of Electrical Engineering and Computer Sciences

University of California, Berkeley



Outline



Ref: Analog Devices ADXL-50

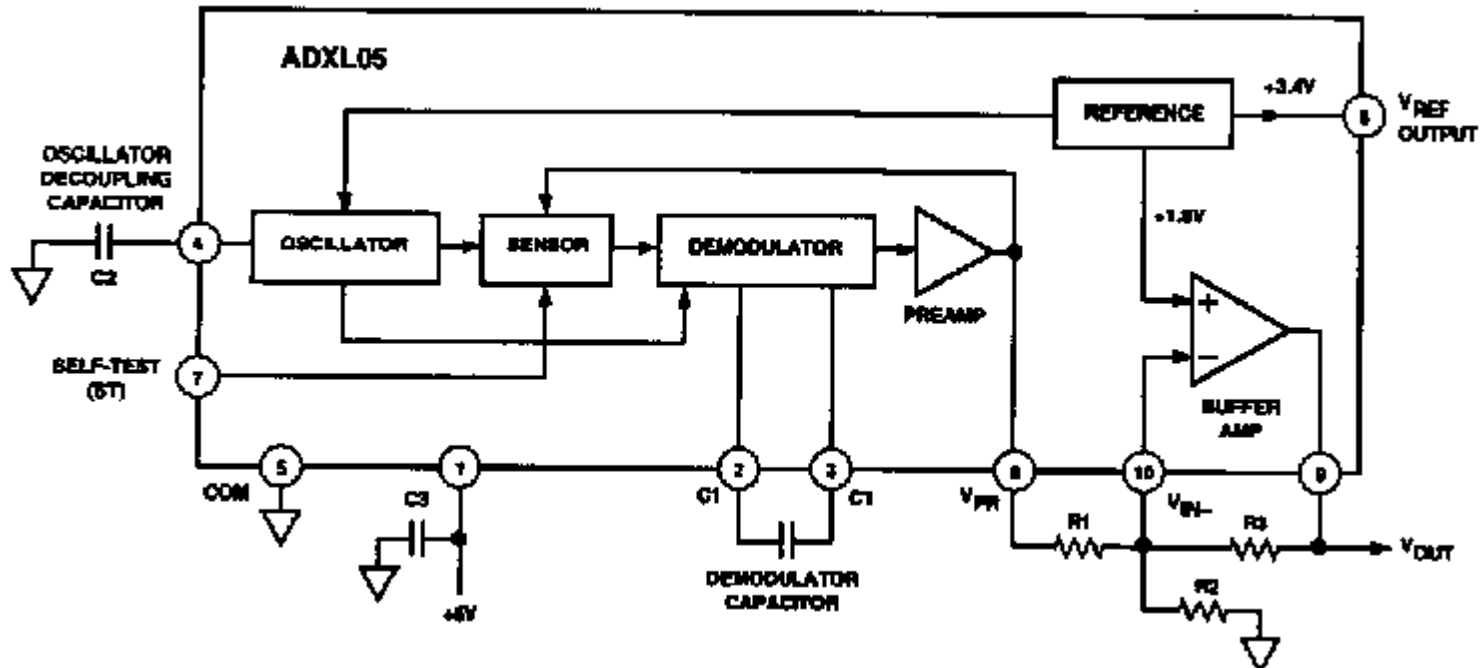
- specifications
- system diagram
- sense element
- force-feedback
- resolution

XL05 Specifications

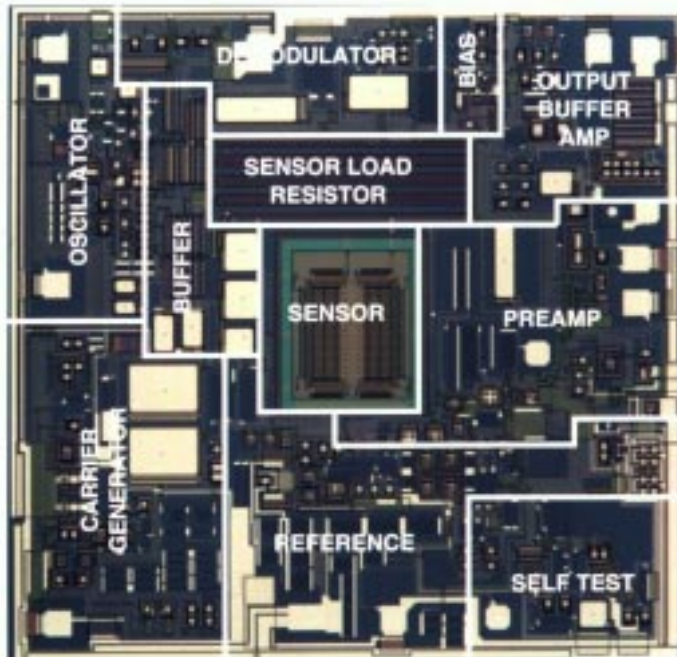
- full scale $\pm 1 \dots 5 g$
- sensitivity $200 \text{ mV/g} \dots 1 \text{ V/g}$
- resolution $5 \text{ milli-g in } 100 \text{ Hz}$ ($1 g = 9.8 \text{ m/s}^2$)
- noise floor $500 \mu\text{g/rt-Hz}$
- bandwidth $1.6 \dots 4 \text{ kHz}$
- resonance 12 kHz
- linearity $0.2 \% \text{ of full scale}$
- off-axis sensitivity $\pm 2 \%$
- alignment error $\pm 1^\circ$
- supply $5 \text{ V}, 8 \text{ mA}$



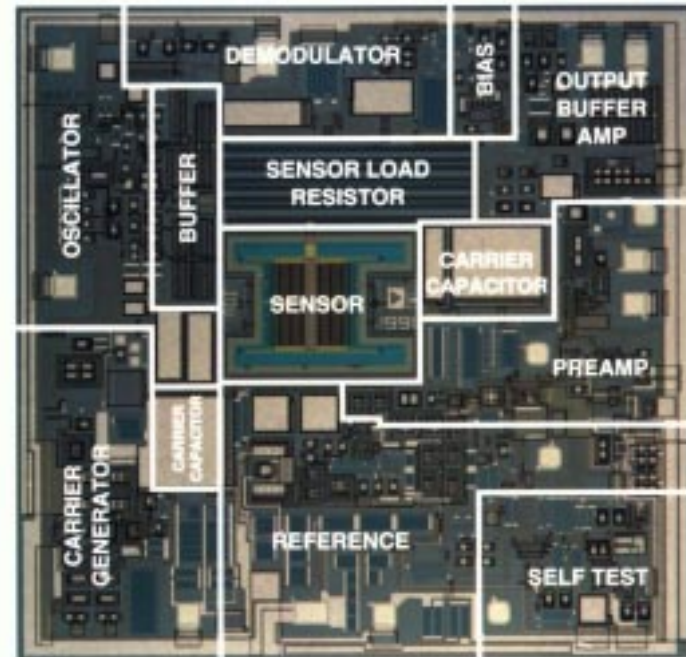
Functional Block Diagram



Layout

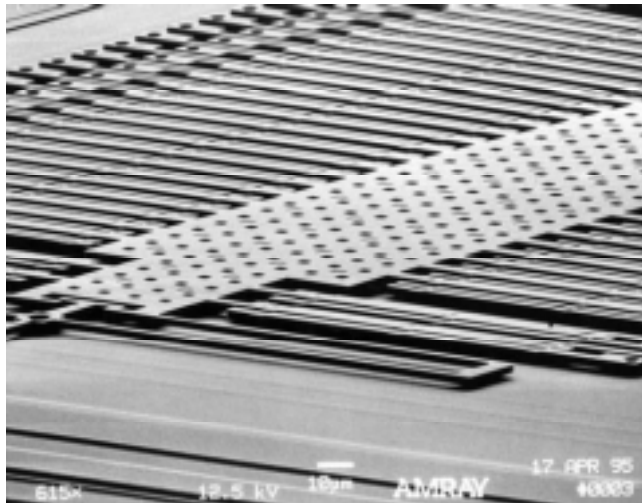


ADXL05

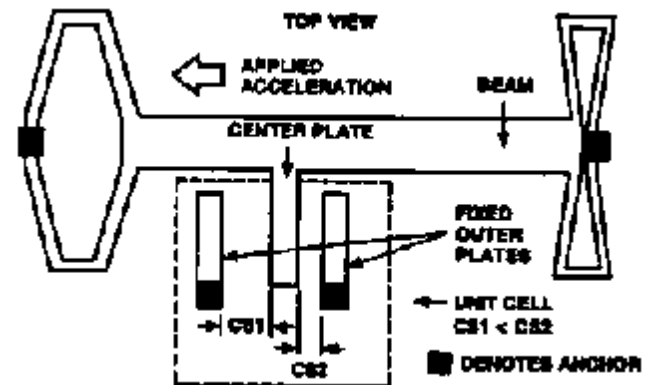
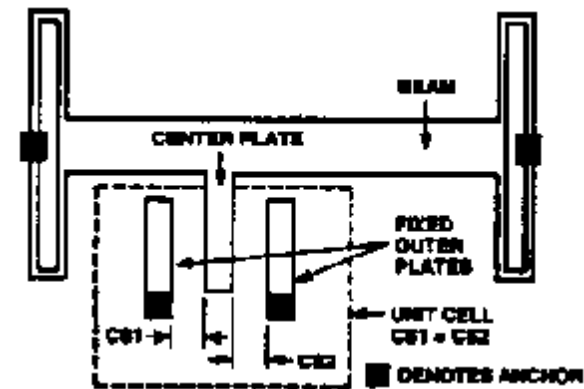


ADXL50

Sense Element

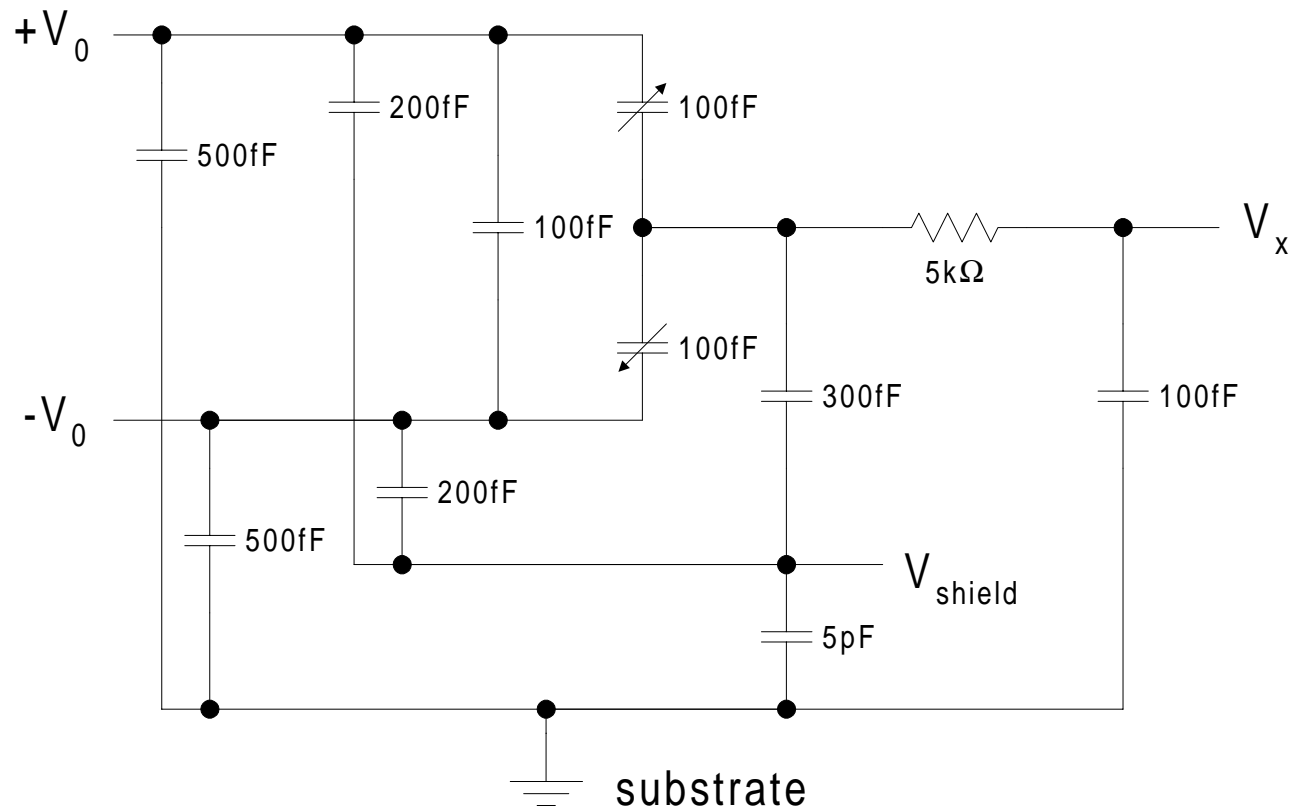


ADXL 05 proof mass.



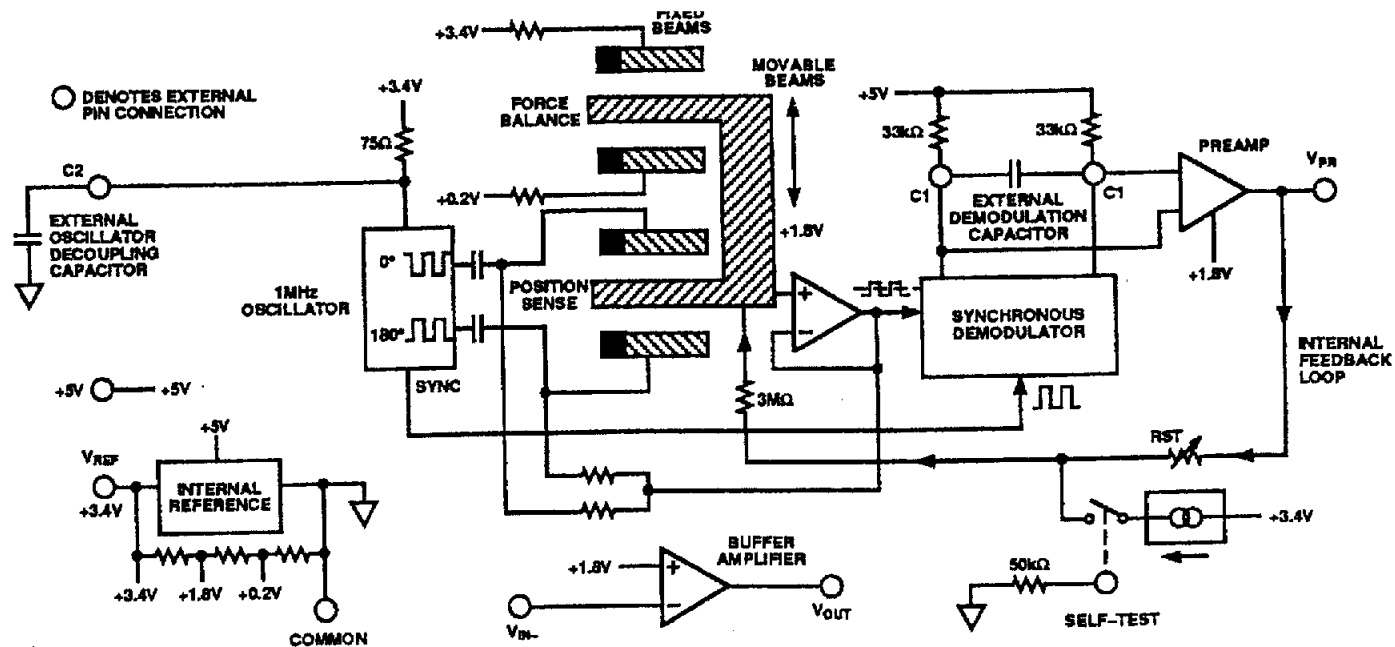
Electrical Interface

(capacitor values estimated)



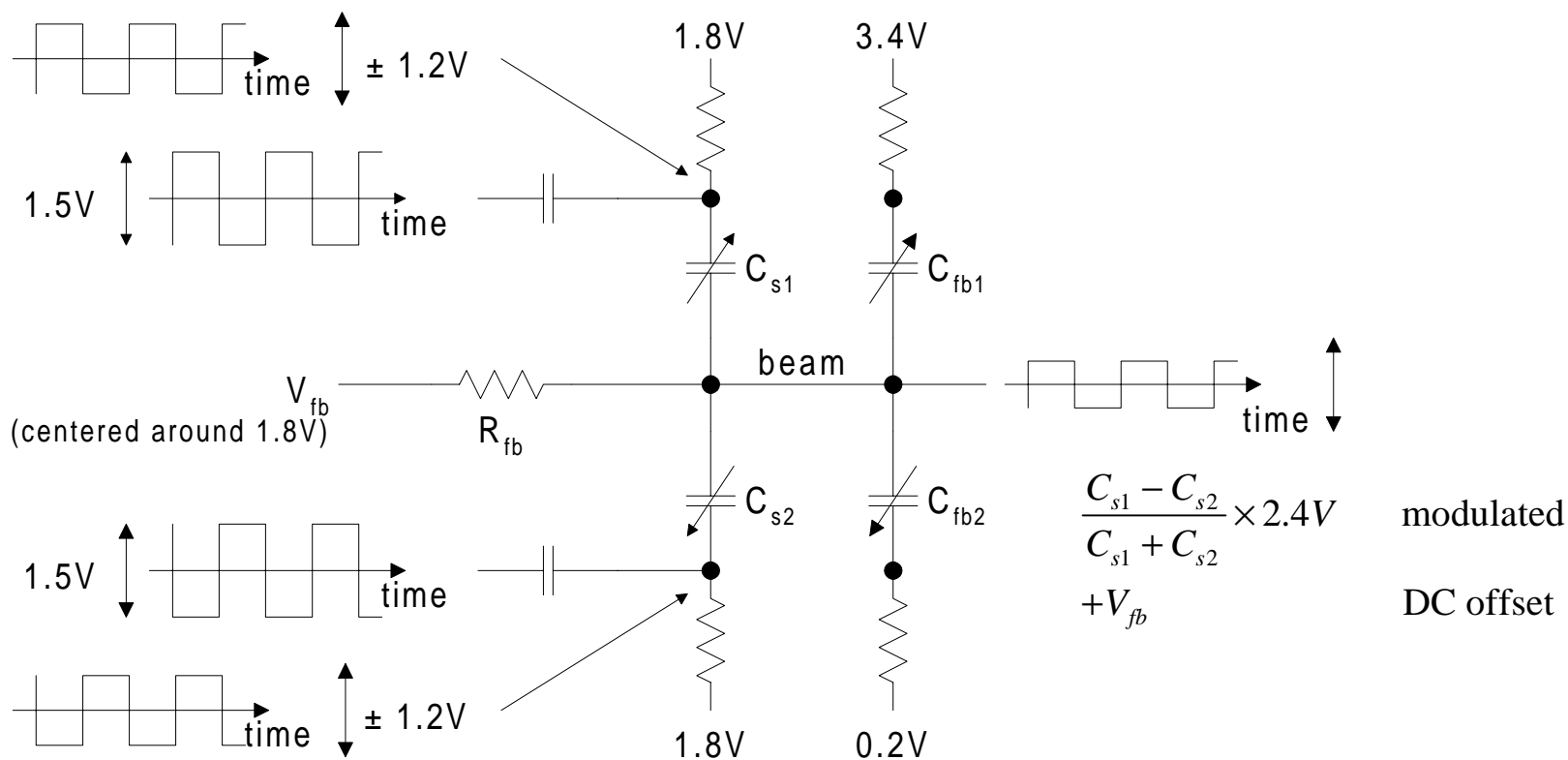
Electrical Block Diagram

XL-05

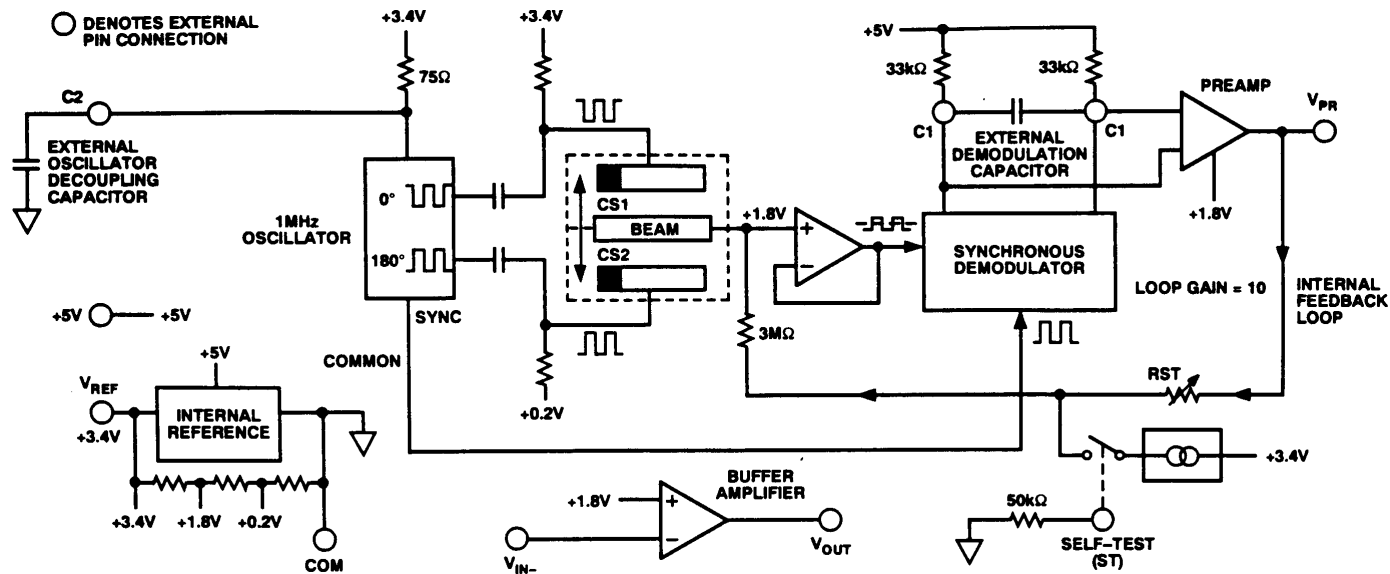


Capacitive Interface

XL-05



Electrical Block Diagram XL-50

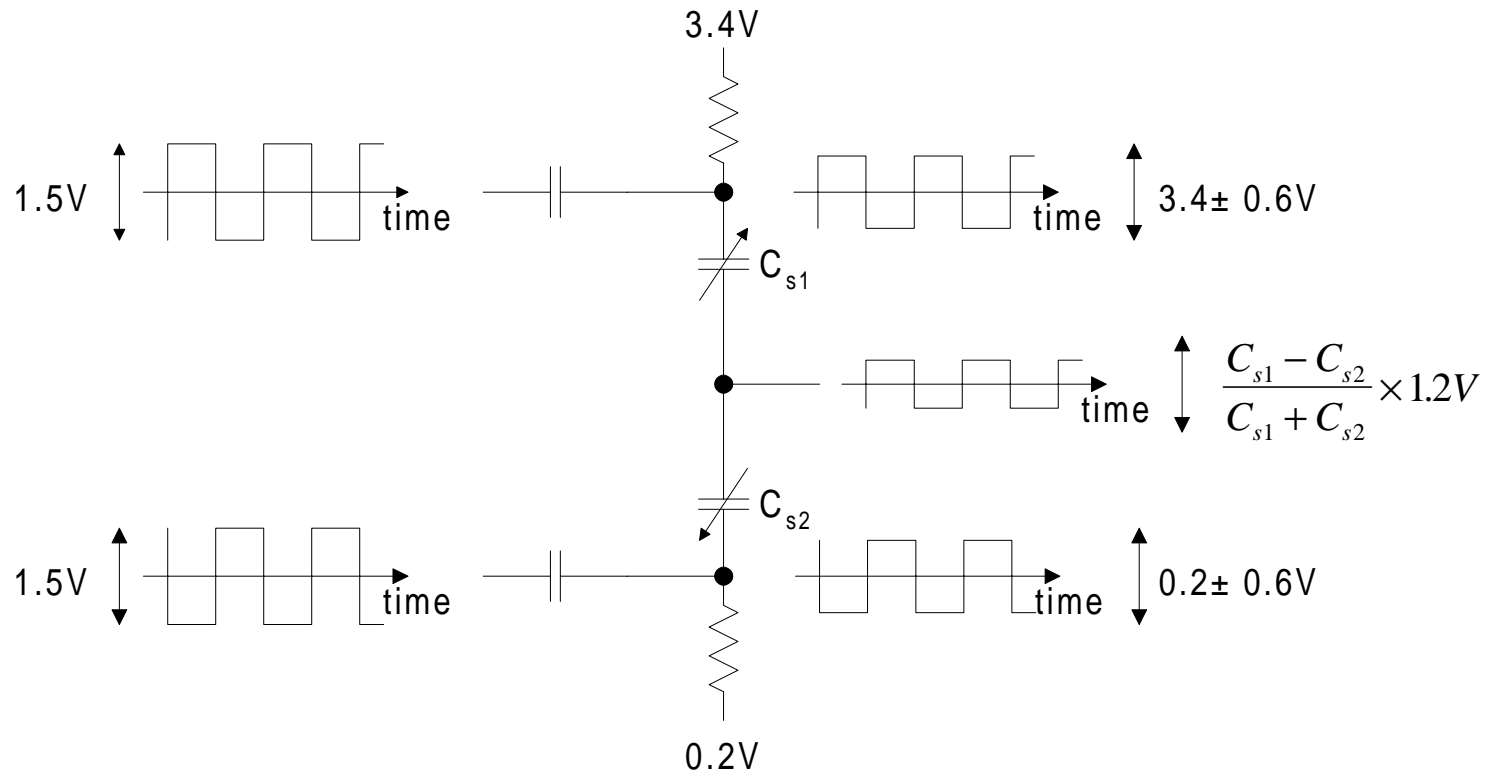


increased input range (50g): use all fingers for feedback
(share with sense operation)



Capacitive Interface

XL-50

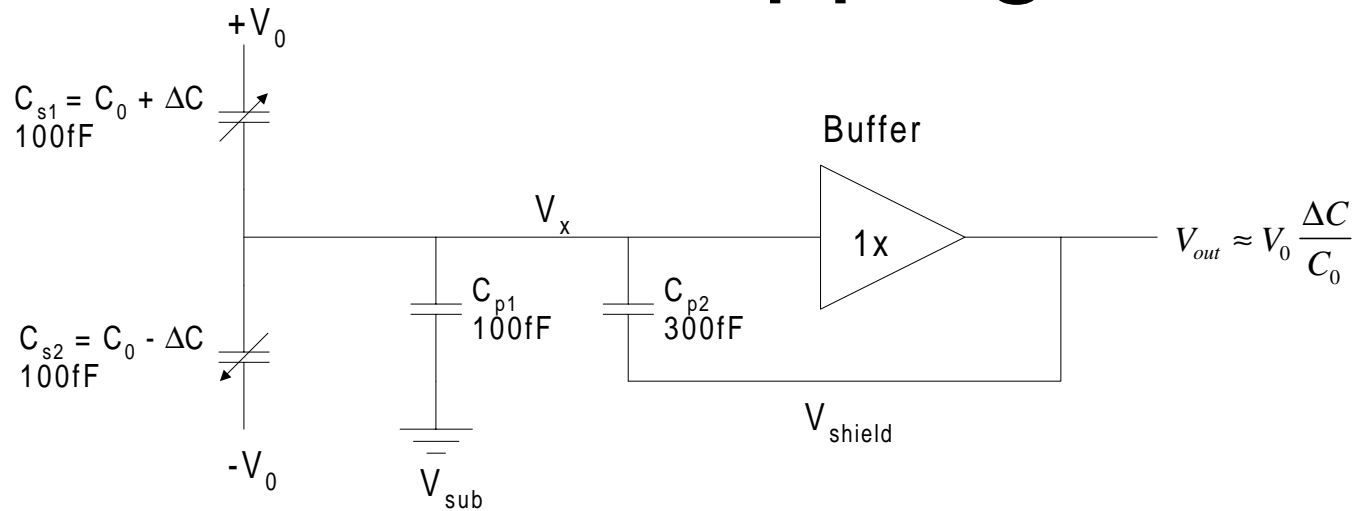


XL-05 vs XL-50 Comparison

	XL-05	XL-50	performance gain
sense voltage (peak-to-peak)	1.2V	0.6V	2x
resonant frequency (increased mass, softer springs)	12kHz	24kHz	4x
increased sense capacitance			1.5x
<i>Total performance improvement of XL-05 over XL-50:</i>			12x



Bootstrapping



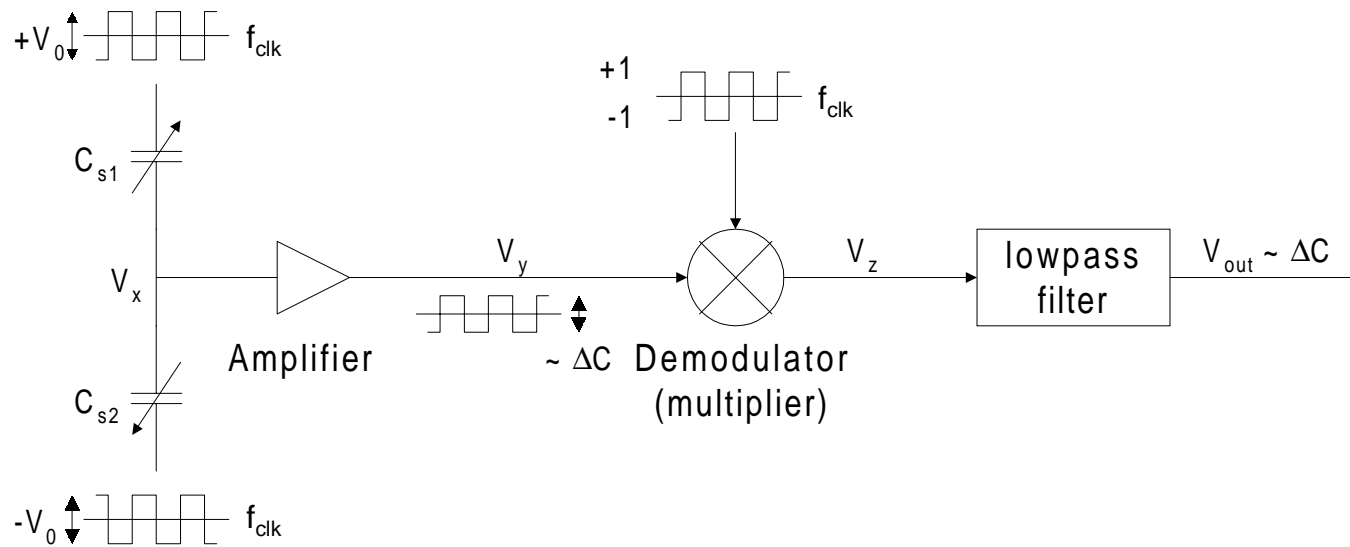
- $V_{\text{shield}} = V_{\text{out}} = V_x$ ----> voltage across C_{p2} is always zero

$$V_x = \frac{2\Delta C V_0 + C_{p1} V_{\text{sub}}}{2C_0 + C_{p1}}$$

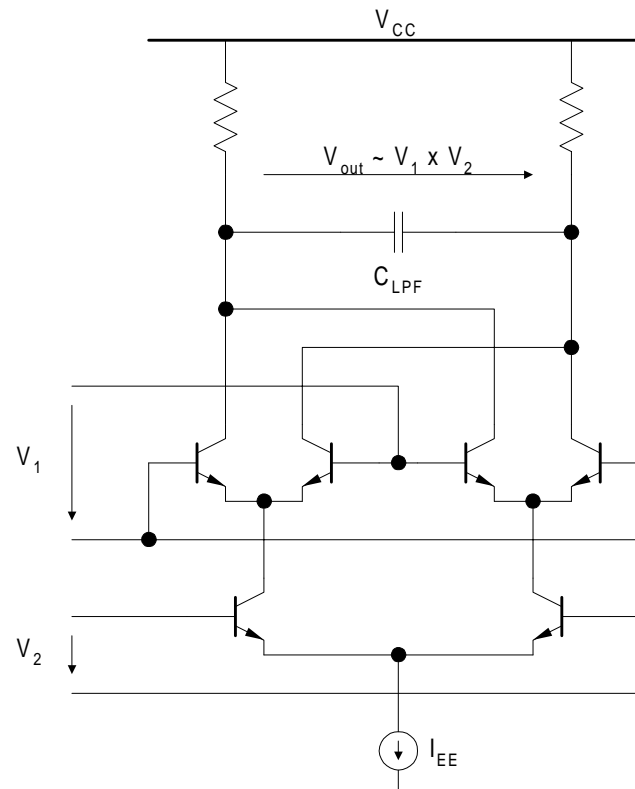
C_{p2} effectively removed



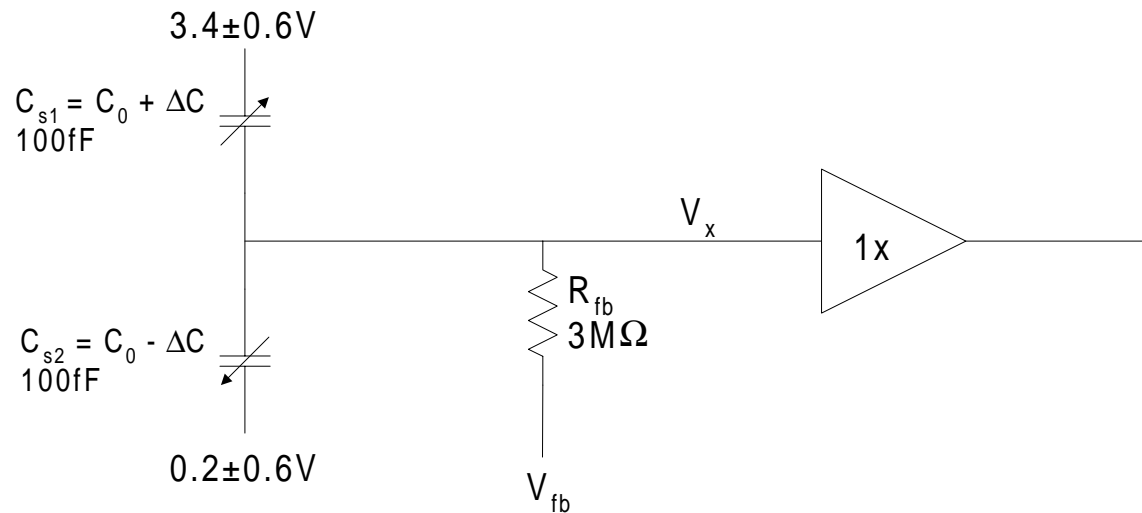
Demodulation



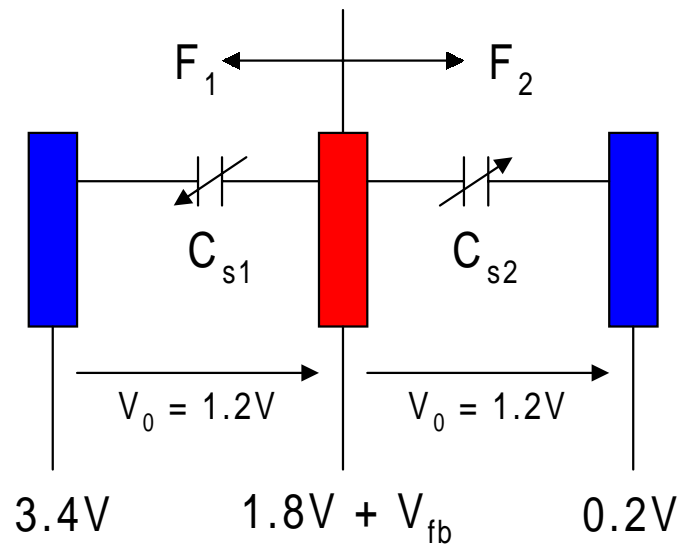
Demodulator & Lowpass Filter



Force-Feedback



Differential Force

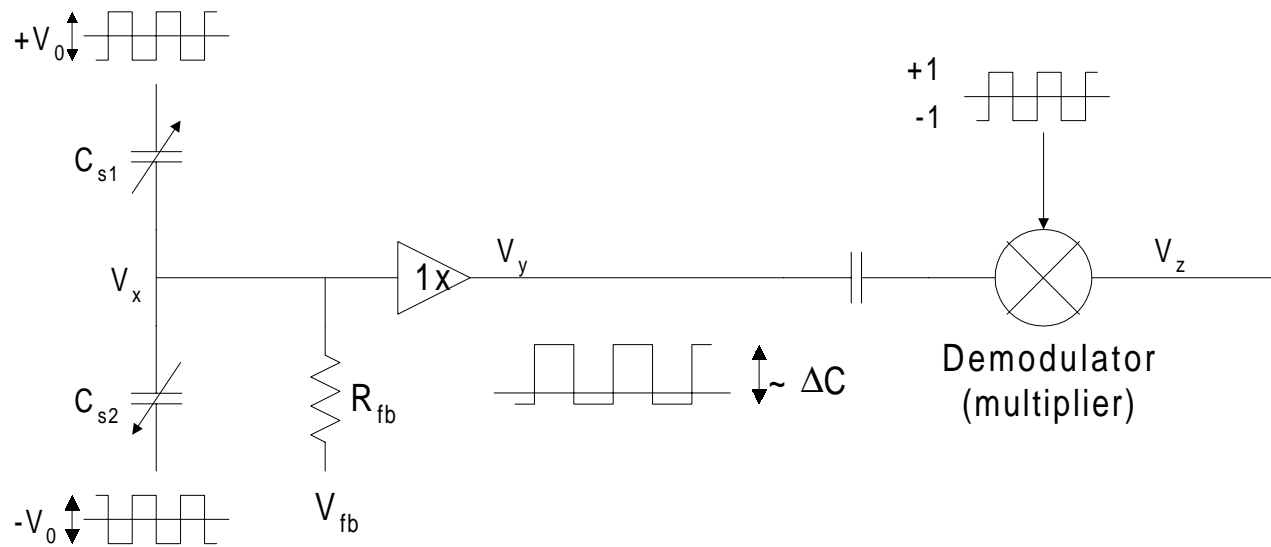


$$\begin{aligned} \Delta F &= F_1 - F_2 \\ &\approx -\frac{1}{2} \frac{C_0}{x_0} \left[(V_0 - V_x)^2 - (V_0 + V_x)^2 \right] \\ &\approx \frac{2C_0 V_0 V_x}{x_0} \quad x \ll x_0 \end{aligned}$$

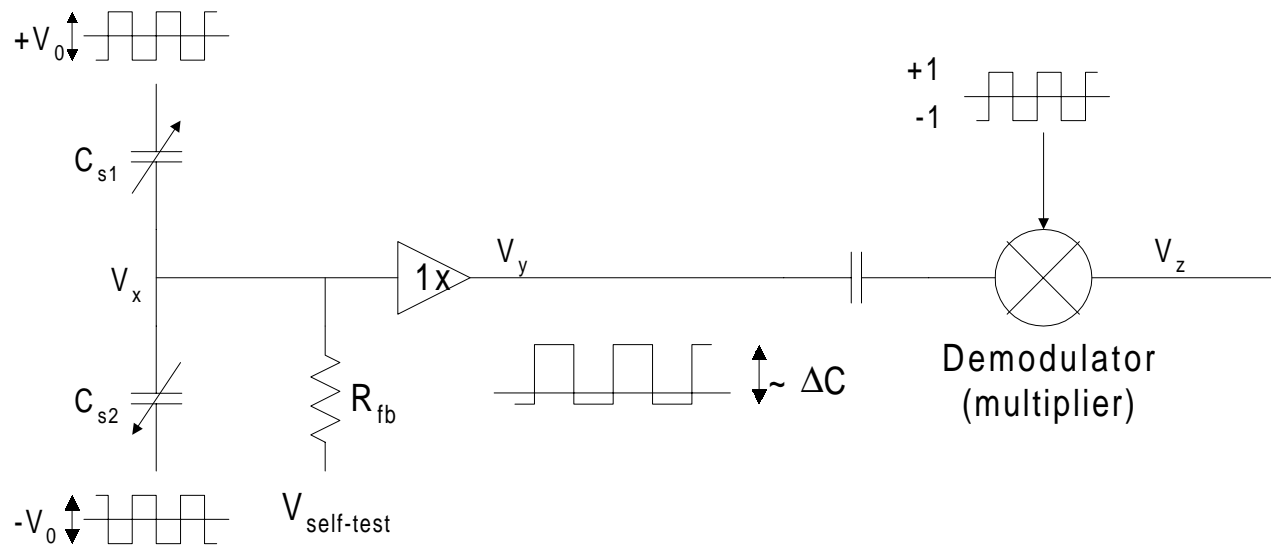
$$\frac{\Delta F}{V_{fb}} \approx 0.1 \mu N / V$$

$$\frac{\Delta a}{V_{fb}} = \frac{1}{m} \times \frac{\Delta F}{V_{fb}} = 1000 g / V$$

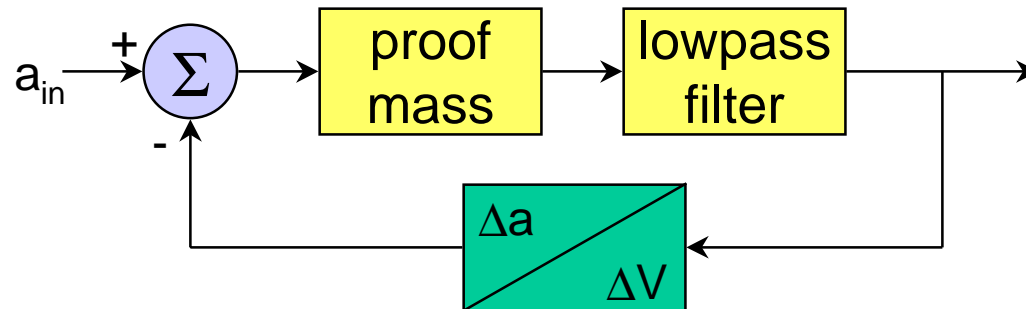
AC Coupling



Self-Test

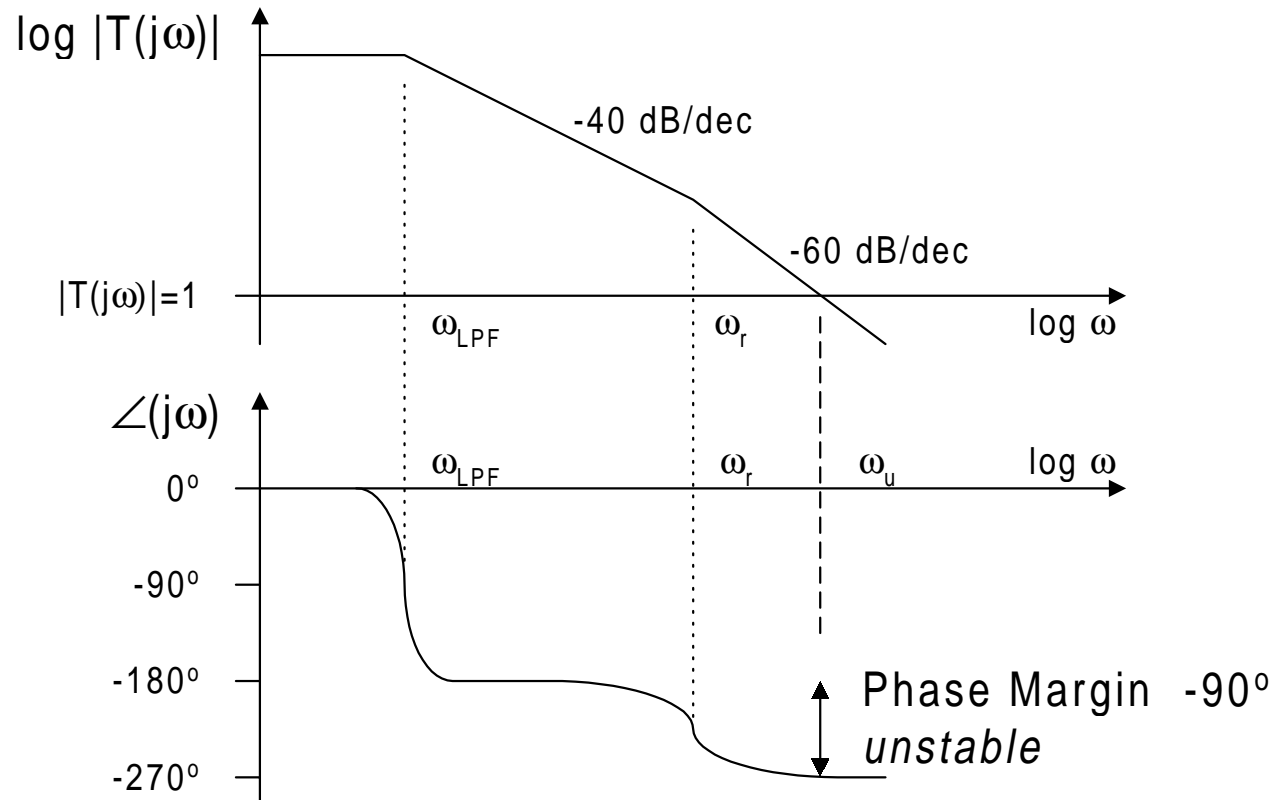


Stability Analysis

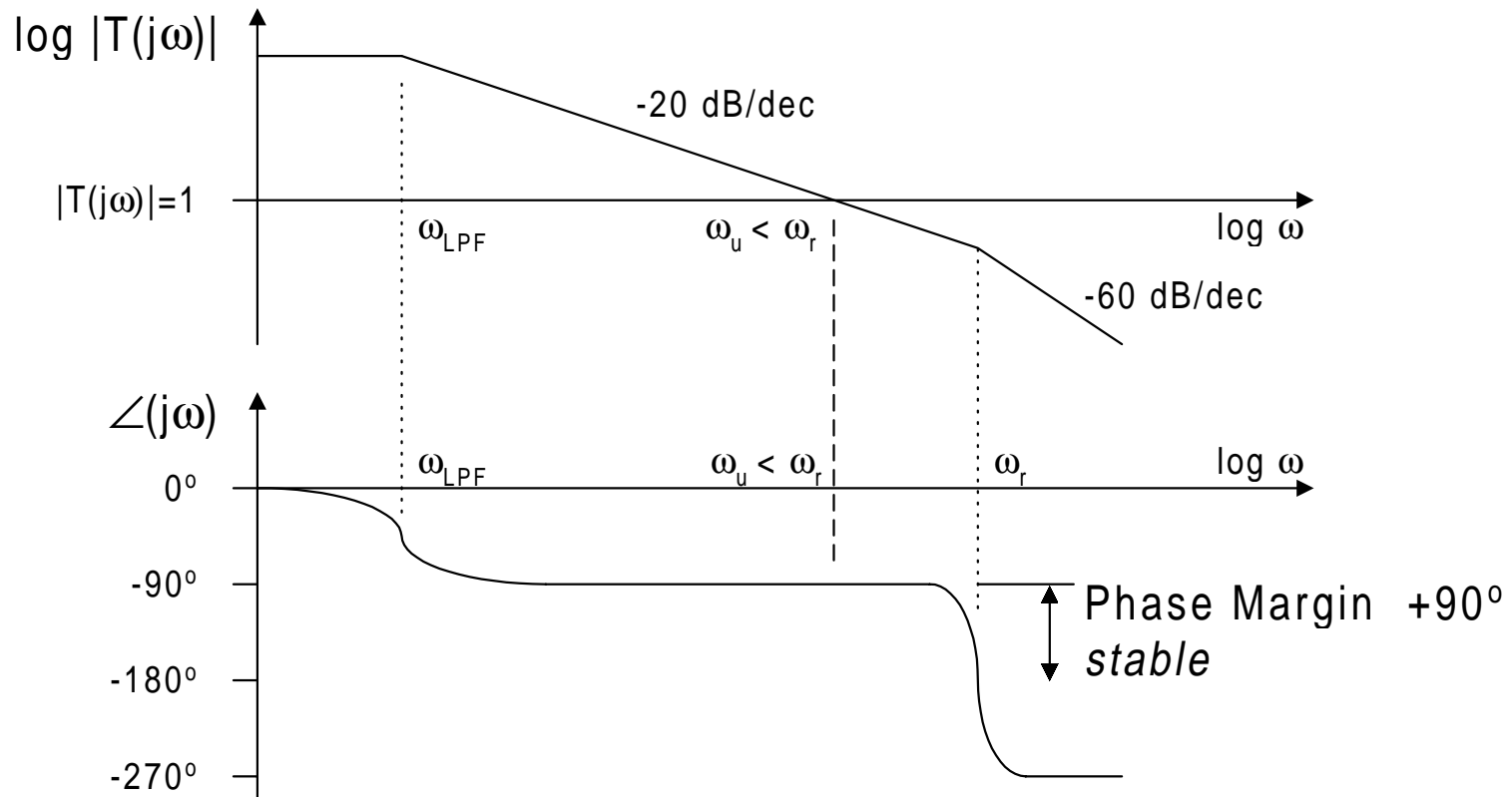


Loop Gain $T(s) = \underbrace{\frac{1}{s^2 + s \frac{\omega_r}{Q} + \omega_r^2}}_{\text{proof mass}} \times \underbrace{\frac{1}{1 - \frac{s}{\omega_{LPF}}}}_{\text{lowpass filter}}$

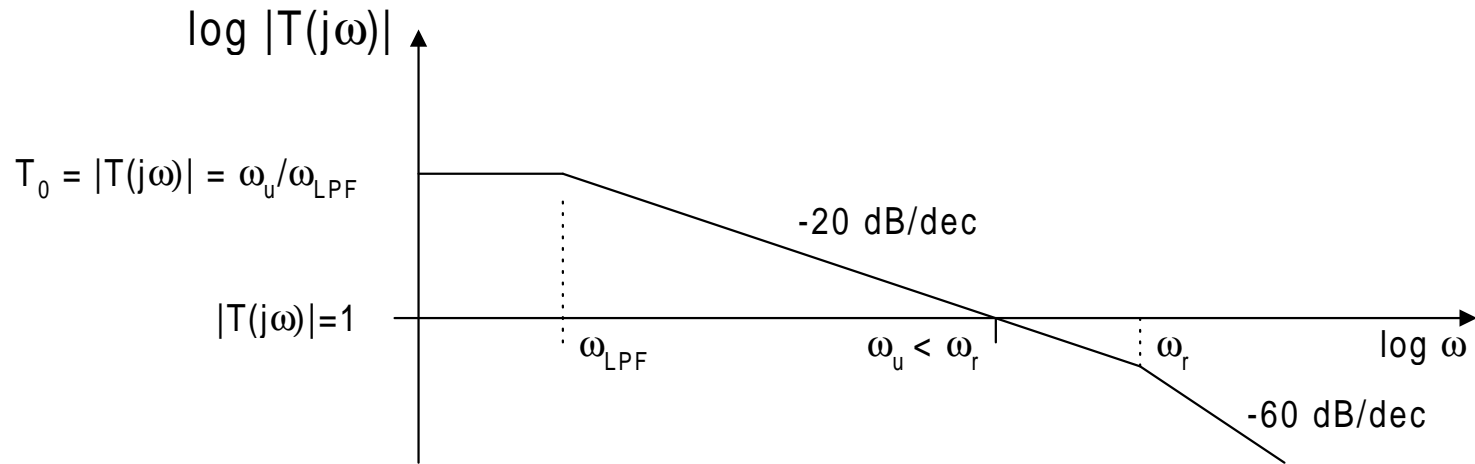
Bode Plot



Narrow-Banding

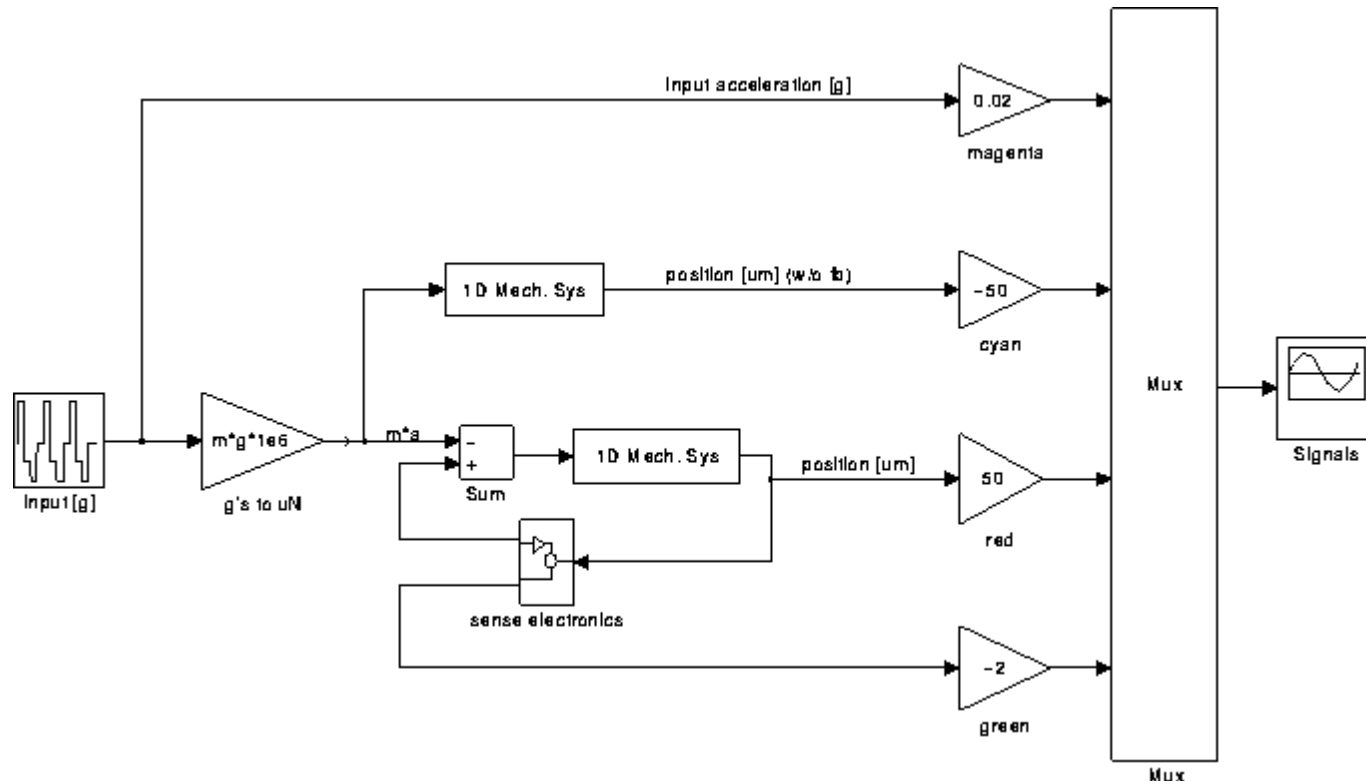


Maximum Loop-Gain

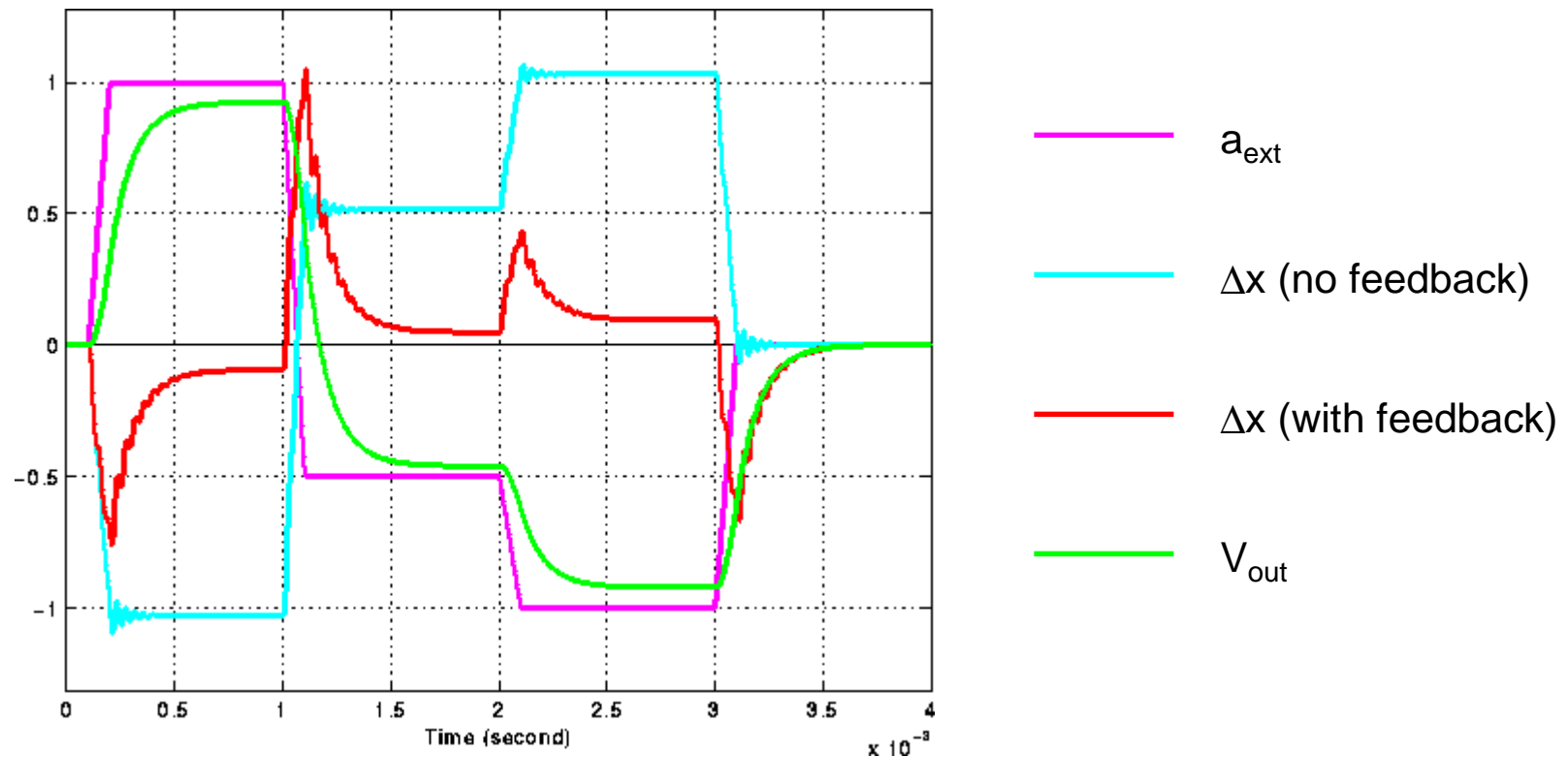


$$\begin{aligned}
 T_0 &= \frac{\omega_u}{\omega_{LPF}} < \frac{\omega_r}{\omega_{LPF}} \\
 &= \frac{f_r}{B} \\
 &= \frac{12 \text{ kHz}}{1 \text{ kHz}} = \underline{12}
 \end{aligned}$$

Matlab Simulation



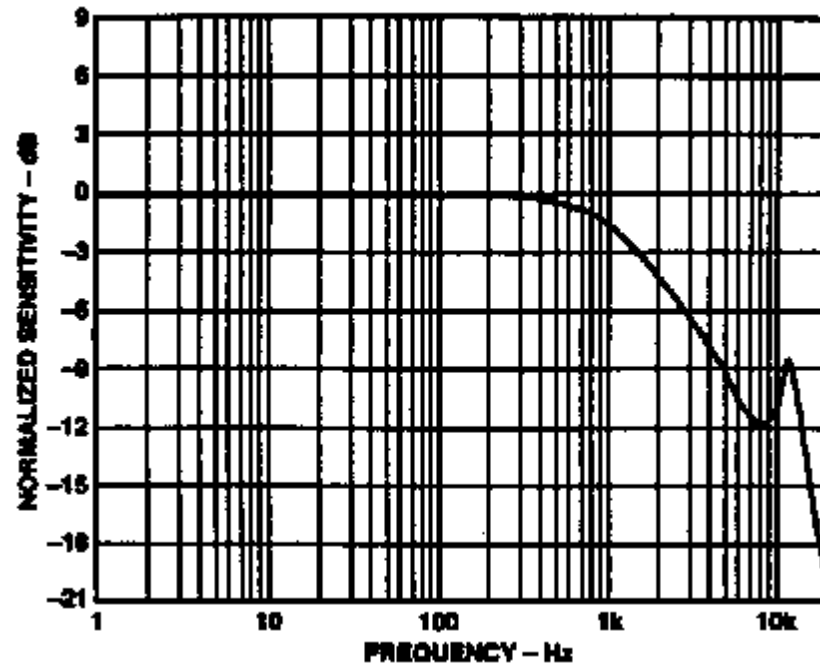
Simulation Result



Δx reduced only by factor $T_0 + 1 = 11$



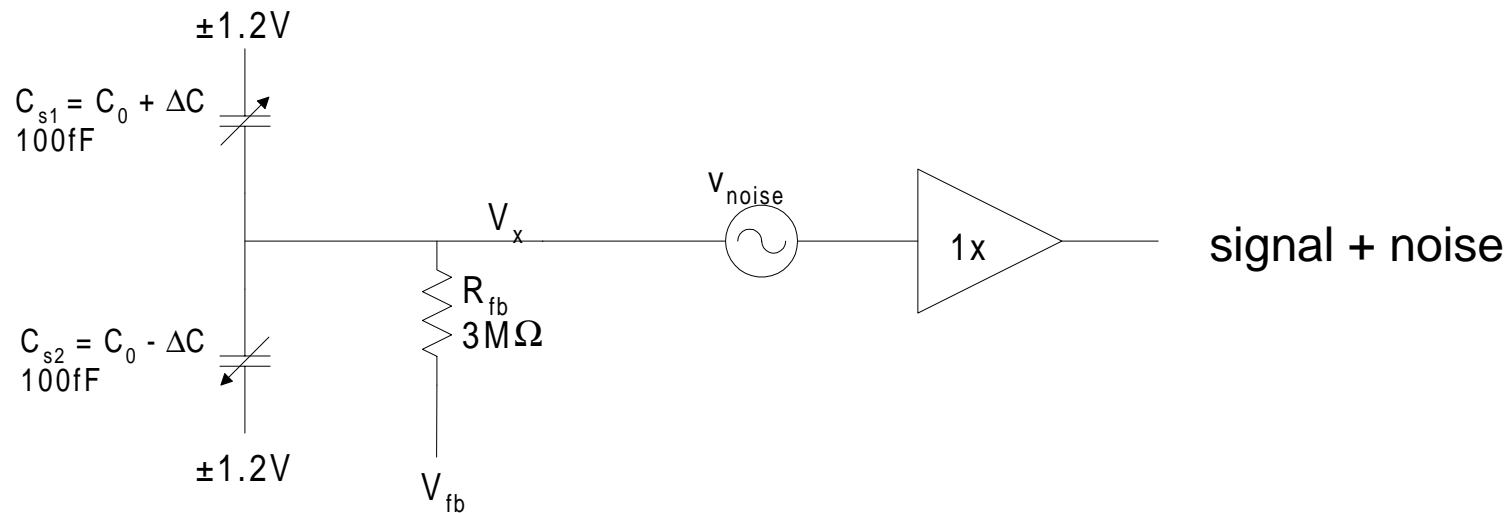
Closed Loop Frequency Response



Resonance peak not attenuated by feedback.



Noise Floor



Noise Analysis

signal amplitude:

$$\begin{aligned}V_x &= V_0 \times \frac{\Delta C}{C_0} \\&= \frac{V_0}{C_0} \times \frac{dC}{dx} \times \Delta x \\&= \frac{V_0}{C_0} \times \frac{C_0}{x_0} \times \frac{\Delta a}{\omega_r^2} \\&= \frac{V_0}{x_0} \times \frac{\Delta a}{\omega_r^2}\end{aligned}$$

signal power:

(assume sinusoidal signal)

$$\overline{v_x^2} = \frac{1}{2} \left(\frac{V_x}{2} \right)^2 = \frac{V_x^2}{8}$$

noise power:

$$\begin{aligned}\overline{v_n^2} &= (S_{amp})^2 \Delta f \\&\approx \left(500 \frac{nV}{\sqrt{Hz}} \right)^2 \Delta f\end{aligned}$$



Minimum Detectable Signal

signal power = noise power

$$\begin{aligned}\sqrt{\frac{(\Delta a)^2}{\Delta f}} &= \sqrt{8} \frac{\omega_r^2 x_0 S_{amp}}{V_0} \\ &\approx \sqrt{8} \frac{(2\pi \times 12 \text{ krad/s})^2 \times 2\mu\text{m} \times 500 \frac{\text{nV}}{\sqrt{\text{Hz}}}}{1.2\text{V}} \\ &= \underline{\underline{350 \frac{\mu\text{g}}{\sqrt{\text{Hz}}}}} \quad \text{Measured: } 600 \mu\text{g/rt-Hz}\end{aligned}$$



Minimum Detectable Displacement

$$\begin{aligned}\sqrt{\frac{(\Delta x)^2}{\Delta f}} &= \sqrt{\frac{(\Delta a)^2}{\Delta f}} \times \frac{1}{\omega_r^2} \\ &\approx 0.0006 \frac{nm}{\sqrt{Hz}}\end{aligned}$$

$$\text{measured: } 0.001 \frac{nm}{\sqrt{Hz}}$$

$$\begin{aligned}\sqrt{\frac{(\Delta C)^2}{\Delta f}} &= \sqrt{\frac{(\Delta x)^2}{\Delta f}} \times \frac{C_0}{x_0} \\ &\approx 3 \times 10^{-20} \frac{F}{\sqrt{Hz}}\end{aligned}$$

$$\text{measured: } 6 \times 10^{-20} \frac{F}{\sqrt{Hz}}$$



Contents of a Can ...

